

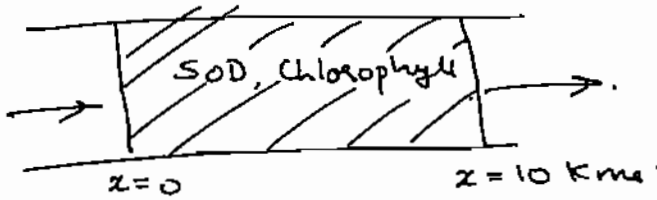
Major Exam 2006 CEL 741 Surface Water Quality Modeling & Control

max marks 60

- Q(1) A river has flow of $10 \text{ m}^3/\text{s}$, a depth of 3 m, and receives a point input of PCB of 1000 g/day. The partition coefficient is 10^5 litres/Kg, average solids concentration is 20 mg/l, and net solids settling velocity is 0.2 m/day. The volatilization loss is 1.5 m/day.
- Calculate the total PCB concentration at travel time=10 days
 - Calculate the dissolved PCB concentration at travel time = 10 days
- Q(2) A lake has the following characteristics:
Volume = 10^{12} m^3 , Depth = 20 m, flow = $2.74 \times 10^8 \text{ m}^3/\text{day}$, suspended solids = 20 mg/l,
Net solids settling velocity = 0.2 m/day, partition coefficient = 10^4 litres/kg.
The dissolved allowable concentration should not exceed $0.06 \mu\text{g}/\text{litre}$
Determine the allowable discharge of this toxicant in kg/year (steady state) assuming dissolved concentration as conservative.
- Q(3) The in-lake phosphorus concentration has been measured at $192 \mu\text{g}/\text{litre}$.
- If the net settling rate of total phosphorus is 12.4 m/yr, the volume is 10^{10} m^3 , the flow is $10^7 \text{ m}^3/\text{day}$ and the depth is 10 m, what is the present total phosphorus loading to the lake in kg/yr?
 - It is desired to have the phosphorus level reduced to $18.2 \mu\text{g}/\text{litre}$. What is the new required total phosphorus loading in Kg/yr?
- Q(4) A shallow well mixed lake receives inputs of phosphorus that resulted in a substantial growth of aquatic plants of all types, causing a DO variation which is unacceptably high. Data is as follows:
Depth = 2 m, flow = $11,000 \text{ m}^3/\text{day}$, total incoming phosphorus = 8030 kg/yr, total phosphorus measured in the lake = 20 mg/litre, surface area = 10^6 m^2 , daily averaged photosynthetic oxygen production rate = 4 mg/ litre-day. Data have also been collected on the relationship between the biomass in the lake and the total phosphorus resulting into the following relationship $P' = P^{0.8}$, where P is the total phosphorus in $\mu\text{g}/\text{litre}$ and P' is the areal chlorophyll level in mg/m^2 . Also $P' = P^* H$, where P^* is the chlorophyll concentration in mg/m^3 and H = depth. The carbon to chlorophyll ratio is 100 and the gross growth rate of the plant biomass is 0.2/day. What is the allowable input phosphorus load in kg/yr to meet this restriction? Assume area, settling velocity and flow to remain constant.

P.T.O.

Q(5) A river has the following characteristics for the stretch from travel time $x=0$ to $x=10$ Kms

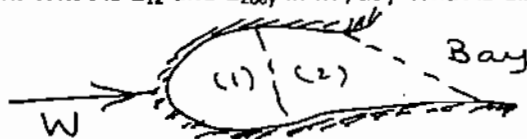


Chlorophyll=20 $\mu\text{g/litre}$, $T=20^\circ\text{C}$, light factor $G(I)=0.44$, $a_{op} = 0.266 \text{ mg DO}/\mu\text{g Chl}$, $G_{max}=1.88/\text{day}$, $C_s=9.1 \text{ mg/litre}$, sediment oxygen demand=3 $\text{gm/m}^2\text{-day}$, aeration rate=0.62/day, effective deoxygenation rate=0.2/day, overall loss rate=0.2/day, photo period=0.5, depth=2m, velocity of flow=1.0 km/day. At $x=0$, the DO deficit=3 mg/litre, and C8ODU=29 mg/litre.

What is the total DO concentration in mg/litre expected at $x=10$ Kms

Q(6) a) An estuary with no net flow receives an input of 10^3 kg/day . The cross sectional area of estuary is 5000 m^2 , $E=5 \times 10^6 \text{ m}^2/\text{day}$ and decay rate=0.1/day. What inflow (in m^3/s) would be required to be discharged to the estuary so that the concentration at the outfall after mixing is reduced by 50% from the concentration at the outfall with no flow in the estuary

b) A harbor of a large bay receives a discharge at one end as shown. The harbor is divided into two segments. A conservative substance is released into segment (1) at 1.0 kg/day . There is no advective flow through the system. What is E_{12} and E_{2bay} in m^3/day What is dispersive flux across interface between segment (2) and bay



$S(1) = 12 \text{ mg/L}$
 $S(2) = 5 \text{ mg/L}$
 $S_{bay} = 1 \text{ mg/L}$

Formulas: $D = D_0 e^{-K_a t^*} + \frac{K_d L_0}{K_a - K_r} [e^{-K_r t^*} - e^{-K_a t^*}] + \frac{(R + S_b' - P_a)}{K_a} (1 - e^{-K_a t^*})$

$P = \frac{W'}{q + U_s}$, $C_T = \frac{W}{Q} e^{-\frac{U_T}{H} t^*}$, $R = 0.1 a_{op} p^* (1.08)^{T-20} p^*$

$P_a = a_{op} G_p p^*$, $a_{op} = 2.67 a_{cp}^*$, $f_d = (1 + K_d m)^{-1}$

$G_T = G_{max} (1.066)^{T-20}$, $\delta = \frac{W}{2A\sqrt{KE}}$, $\delta = \frac{W}{Q\sqrt{1+4KE/U^2}}$

$s = s_0 e^{j_1 x}$, $j_1 = \frac{U}{2E} (1 + \alpha)$, $\alpha = \sqrt{1 + 4KE/U^2}$
 $= s_0 e^{j_2 x}$, $j_2 = \frac{U}{2E} (1 - \alpha)$

$U_T = K_1 H_1 + U_v f_{d1} + (U_s f_{p1} + U_e f_{d1}) (1 - F_r')$

$F_r' = (U_u + U_e f_{d2}) / (U_u + U_e f_{d2} + U_d + K_2 H_2)$